# COOPERATIVE AGREEMENT NUMBER DAMD17-95-2-5007

TITLE:

Crystallization, X-ray Structure Determination and Structure-Based Drug Design for Targeted Malarial Enzymes

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REPORT DATE: July 1998

TYPE OF REPORT: Annual

PREPARED FOR:

Commander

U.S. Army Medical Research and Material

Command

Fort Detrick, Frederick, Maryland 21702-5012

DISTRIBUTION STATEMENT: Approved for public release, distribution unlimited

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### REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gethering and meintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for information Operations and Reports, 1715 defferson Devis Highway, Suite 1204, Arington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503. 3. REPORT TYPE AND DATES COVERED 1. AGENCY USE ONLY (Leave blank) 2. REPORT DATE Annual (15 Jun 97 - 14 Jun 98) July 1998 \_\_ 4. TITLE AND SUBTITLE **6. FUNDING NUMBERS** Crystallization, X-Ray Structure Determination and DAMD17-95-2-5007 Structure-Based Drug Design for Targeted Malarial 6. AUTHOR(S) Lawrence J. DeLucas, Ph.D. 8. PERFORMING ORGANIZATION 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) REPORT NUMBER University of Alabama at Birmingham Birmingham, Alabama 35294-0111 9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING/MONITORING Commander AGENCY REPORT NUMBER ' U.S. Army Medical Research and Materiel Command Fort Detrick, Frederick, Maryland 21702-5012 11. SUPPLEMENTARY NOTES 19990301006 12a. DISTRIBUTION / AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Approved for public release; distribution unlimited 13. ABSTRACT (Maximum 200 The goal of this project is to design selective anti-malarial compounds using a structure-based inhibitor design approach. Several potent inhibitors of Plasmodium falciparum lactate dehydrogenase have been identified. We are in the process of crystal structure analysis of the enzyme-inhibitor complexes. Attempts to determine the structure of the catalytic domain of Rab6 is in progress. Enzymatic characterization of monofunctional dihydropteroate synthetase will be done before crystallization effort is initiated. 15. NUMBER OF PAGES 14. SUBJECT TERMS 12 16. PRICE CODE 17. SECURITY CLASSIFICATION 18. SECURITY CLASSIFICATION 19. SECURITY CLASSIFICATION 20. LIMITATION OF ABSTRACT

Unclassified NSN 7540-01-280-5500

OF REPORT

Unlimited Unclassified Standard Form 298 (Rev. 2-89) Prescribed by ANSI Std. Z39-18 298-102

OF ABSTRACT

OF THIS PAGE

Unclassified

#### **FOREWORD**

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Larry J. Le Lucas 1/13/96
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#### 1. Introduction:

Infection with malaria parasite still remains the most deadly infection causing approximately 1.5 million deaths worldlwide (1). The disease is caused by the parasites of Plasmodium species and is transmitted by certain strains of mosquito. Majority of the deaths and clinical complications of malaria are due to infection with P. falciparum, the most lethal of the four Plasmodium species. Although intense effort to produce a useful vaccine against malaria still continues, the results so far has not been rewarding. Malaria is currently treated by chemotherapy. The usefulness of available chemotherapeutic agents is seriously compromised by the development of drug resistant parasite strains (2). There is urgent need for developing new and potent anti-malarials (3). We have undertaken a rational approach for the development of anti-malarial agent using structure-based drug design. This technique will enable us to identify active site inhibitors of several key enzymes of the parasite. Targeting the active site of important metabolic enzymes reduces the likelihood of eventual resistance due to genetic mutation. Also, attacking several key enzymes in a combination therapy and simultaneous development of new generation of inhibitors will be useful in long term treatment. Lactate dehydrogenase (LDH) enzyme is essential for the life cyle of the malaria parasite and compounds that inhibit LDH will also kill the parasite (4). In collaboration with scientists at WRAIR we have identified some lead inhibitors of the Pf LDH. In a structure-based drug design project high resolution three domensional structure of the enzyme - inhibitor complex provides the basis for further modifications of the inhibitor in order to optimize the favorable interactions with the protein molecule (5, 6). We have begun structure analysis of the LDH-inhibitor complexes.

## 2. Experimental Methods, Assumptions, Procedures, Results and Discussion

Lactate Dehydrogenase

Characterization of potent inhibitors, crystal structure analysis of enzyme-inhibitor complexes.

We have determined the structure of the *P. falciparum* LDH at 2.0A resolution using molecular replacement method. We have been working closely with the scientists at WRAIR to identify and characterize *pf* LDH inhibitors using the available chemical library at WRAIR. This approach has been very successful and our collaborators (Capt. Karl Weborvitz and others) have identified several *Pf* LDH inhibitors with IC<sub>50</sub> in the micromolar range. One of these compounds inhibited the growth of erythrocyte

stage P. falciparum with an  $IC_{50}$  of about 15  $\mu g/ml$ .

We have now intesified our effort on LDH. A post doctoral fellow (Dr. D. Prahadeewaran) has been recently recruited to work full-time on the structure determination of LDH-inhibitor complexes under the supervision of Dr. Debasish Chattopadhyay. Once the condtions for preparing the crystals of the enzyme-inhibitor complex is established, structure determination can be completed relatively rapidly since the crystal structure of the native enzyme is already known. The recombinant protein has already been crystallized in the presence of the WRAIR inhibitor BK19981. To prepare the complex the protein was incubated with 2 mM BK19981 and 3.2 mM NADH at 4°C for 3 hrs. The resulting mixture was crystallized at 4°C using hanging drop vapor diffusion technique. The precipitant used was polyethylene glycol 1000. Crystals large enough for X-ray diffraction analysis grows overnight. Crystals of *Pf* LDH - oxamate complex grown under similar conditions diffracted to about 1.7A. Diffraction data for the putative BK19981 complex crystals are currently being collected at -170°C. These crystals also diffract to 1.8A resolution. The crystals are isomorphous with the crystals of the oxamate complex. The unit cell parameters are 79.61, 86.01 and 91.06A and the crystal space group is I222.

#### Sequestrin:

Two new constructs of sequestrin were prepared by Dr. Chris Ockenhouse of WRAIR. We have purified the recombinant protein to homogeneity and used the purified protein for screening crystallization conditions. This effort was not successful.

Falcipain:

Amino acid requirements for protein synthesis in the erythrocytic parasite are fulfilled by degradation of erythrocyte hemoglobin in acidic food vacuole. The cystein protease falcipain has been shown to be necessary for hemoglobin degradation and is therefore, a potential target for antimalarial drug design. Falcipain belongs to papain family of cysteine proteinase. The predicted molecular mass for the mature falcipain is 26.8 kDa.

Dr. Chattopadhyay laboratory worked closely with Dr. Phil Rosenthal's group at the University of California at San Francisco on this project. While Dr. Chattopadhyay's laboratory focussed on the preparation of expression constructs of falcipain in yeast system, Dr. Rosenthal's group participated in characterization of the clones. A large number of clones in several yeast expression vectors were isolated, transformed into respective yeast hosts and transformants were grown in suitable culture medium for expression. The culture media (for secretory constructs) or the cell free extract (for intracellular constructs) were tested for overexpression of falcipain. Overall result of this effort has been unsucessful.

We have recently known that Dr. Virendra Chowhan at New Delhi, India has been successful in expressing an active falcipain in *E. coli*. This has created new enthusiasm in this project and Dr. Chattopadhyay and Dr. Rosenthal are in the process of initiating this new collaboration.

#### Rab6:

Malaria parasite spends much of its life cycle indside erythrocytes. Within the erythrocyte the parasite is surrounded by its own plasma membrane, parasitophorous vacuole membrane, and the cytoplasm and plasma membrane of the erythrocyte. Mechanisms by which proteins are trafficed within and beyond the plasma membrane is not clear. Several components of the standard eukaryotic trafficing mechinery are known to be present. On the other hand, the trafficking machinery of *Plasmodium* possesses distinctive features as well. Rab proteins are small GTP binding proteins. The cytoplasmic surface of each compartment along the secretory pathway appears to have its own unique Rab proteins. The Rab's alternate between GTP-bound and GDP-bound form. They also alternate between cytosolic and membrane bound forms. They appear to act as timers that regulate the kinetics of transport vesicle docking and fusion with target membranes. Cycling of Rab proteins is regulated, at least in part, by a GDP dissociation inhibitor (GDI) and a GDP/GTP exchange protein (GDS).

Recombinant Rab6 was expressed with an amino terminal extension peptide which was designed to facilitate purification of the recombinant protein from the crude bacterial extract using immobilized metal affinity chromatography. The purified protein was crystallized at room temperature. These crystals belong to the space group  $P4_12_12$  with a = b = 82.1, c = 90.87A. Complete native data were collected at a resolution of 2.7A (at -170°C). Attempts to determine the structure using human ras, Rap2A and rac1 structures as search model were not successful.

We have then expressed and purified a new construct of the protein without any extension peptide. This new construct crystallized in the space group  $P4_122$ , with unit cell parameters a=b=79.99, c=88.89 A. Native data to about 2.4A resolution (99% complete) were collected. Attempts to solve this structure by molecular replacement were also unsuccessful. We are now concentrating our effort to determine the structure of this construct using multiple isomorphous replacement method. This will involve soaking native crystals into solutions of various heavy atom reagents and collecting diffraction data

in order to identify useful heavy atom derivatives. At least two independent heavy atom derivatives are required for determining the phase accurately by using this technique. Table 1 summarizes the statistics of the intensity data.

We have also expressed the putative GTPase domain (amino acids 1 - 175) of Rab6. This domain has been purified and crystallized. These crystals also belong the tetragonal space group  $P4_122$  with unit cell parameters a = b = 81.21, c = 90.18 A. We have attempting to solve the structure of this domain by molecular replacement. Several GTPase structures will be used as search model. A summary of statistics of the intensity data is given in Table 2. Attempts to prepare the complex of Rab6 with non-hydrolyzable GTP analog, GTP $\gamma$ S, is also underway.

See Tables 1 and 2.

#### Dihydropterorate synthetase:

DHPS fragment of PPPK-DHPS cloned into pQE30 vector, resulting in 9 additional amino acids at the amino terminus (underlined). This corresponds to aa 379 to 706 of the PPPK-DHPS molecule (6).

mrashhhhhh	kdrisylkek	tnivgilnvn	ydsfsdggif	vepkravqrm	50
	idiggessap				100
kivkcdakpi	isidtinynv	fkecvdndlv	dilndisact	nnpeiikllk	150
kknkfysvvl	mhkrgnphtm	dkltnydnlv	ydiknyleqr	lnflvlngip	200
ryrilfdigl	gfakkhdqsi	kllqnihvyd	eyplfigysr	krfiahcmnd	250
qnvvintqqk	lhdeggnenk	nivdkshnwm	fqmnymrkdk	dqllyqknic	300
gglaiasysy	ykkvdlirvh	dvletksvld	vltkidqv		338

Vector: pQE30

Host: XL-1 Blue

Cloning Sites: Bam H- Hind III

Insert Size: 1047bp

Internal six base cutters. Bgl II @nt#900

Calculated molecular weight: 39.4

Migrates as: 42-45 kDA protein

Growth conditions:

Starting with a single colony, grow 1 Lt over night culture of LB at 37° C. No induction is necessary. After 14-16 hr growth, harvest the cells by centrifugation at 3000xg for 10 min, and resuspend the bacteria in 50 ml of phosphate buffer (50 mM, pH 8.0).

#### Protein extraction and purification:

Break the cells by french press or sonication, and centrifuge the resultant solution at 20,000 rpm for 10 min. Discard the supernatant. Scoop the pellets into a beaker, add 50 ml of 8 M urea in phosphate buffer. Stir at room temperature for 1 hr at low speed. Centrifuge at 20,000 rpm for 30 min, collect the supernatant. Load the supernatant on a 20 ml Ni NTA column (Qiagen) equilibrated with phosphate buffer

containing 8 M urea. Collect and save the flow through (to determine unbound protein). Wash with 100 ml of 50 mM phosphate buffer with 8 M urea first at pH 8.0 and then at pH 6.4. Elute with 100 ml phosphate buffer 50 mM, with 8 M urea at pH 4.5. All these steps can be carried out at room temperature.

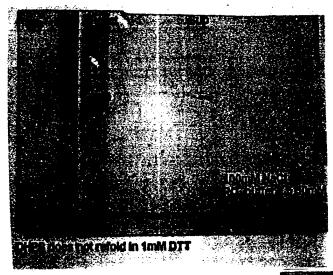
#### Protein refolding:

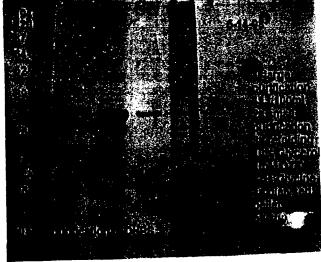
Add  $\beta$  mercaptoethanol to the eluted protein to make it 10 mM final concentration. Dialyze the 100 ml against 4 Lt of 50 mM phosphate buffer, pH 7.5, 100 mM NaCl, 10 mM  $\beta$  mercaptoethanol, 2 M urea and 10% glycerol in cold. After overnight dialysis, dilute the protein to a concentration of 10  $\mu$ g/ml. Extensively dialyze against same buffer without urea.

Centrifuge the dialysate at 20,000 RPM for 10 min. Collect the pellet and resuspend in 50 mM phosphate pH 7.5, 100 mM NACL, 10 mM mercaptoethanol.

The total yield is 10-12 mg/L.

A photomicrograph of a gel showing the purity follows below.





#### 3. Conclusions:

We have entered the most exciting stage of a structure-based drug design project with Pf LDH. Often, finding the first lead inhibitor is a major bottleneck. Fortunately, we have already identified several inhibitors with  $IC_{50}$  in the micromolar range. One of these inhibitors also showed inhibited the growth of the erythrocyte-stage P. falciparum. We have already started cocrystallization of these inhibitors with recombinant enzyme. At this stage, crystal structure of the LDH in complex with lead inhibitors will be determined. Information gathered from these structures will be used to chemically modify the compounds so as to optimize the binding with the enzyme. We have already crystallized the full length and the GTPase domain of Pf Rab6. Attempts are underway to determine the structure of the GTPase domain using molecular replacement technique. If this approach does not produce useful solution we will concentrate on traditional multiple isomorphous replacement method. We have designed a protocol for purification and refolding of monofunctional DHPS. The refolded protein will be assayed for enzymatic activity. If this construct is found active, we will proceed with crystallization of the protein.

#### 4. Plans for next year:

- a. Crystal structure analysis of LDH inhibitor complexes. Exchange the results with scientists at WRAIR, coordinate directed library search for identifying more potent inhibitors. Prepare and supply active enzyme for conducting inhibitor screens.
- b. Determine and refine structure of Pf Rab6.
- c. Assay enzymatic activity of recombinant DHPS and ,if active, crystallize the protein for structure analysis.

Table 1

```
I/Sigma in resolution shells:
shell
                     No. of reflections with I / Sigma less than
  Lower Upper
                                                             20
                                                                    >20
                                                                           total
                                          3
                                                       10
                                   2
                            1
  limit limit
                                                 92
                                                       146
                                                              358
                                                                    1153
                                                                            1511
                                         61
                                  43
                           30
          4.87
                    13
  99.00
                                                       157
                                                              350
                                                                    1092
                                                                            1442
                                                 95
                                  48
                                         61
                           27
          3.86
                    12
   4.87
                                                                     829
                                                       277
                                                              589
                                                                            1418
                           28
77
                                               131
                                  53
                                         78
                    10
          3.37
   3.86
                                                                     536
                                                                            1397
                                                       494
                                                              861
                                               302
                                 152
                                        211
          3.07
                    34
   3.37
                                                       782
                                                             1185
                                                                     207
                                                                            1392
                                                456
                                 197
                                        285
                          102
          2.85
                    36
   3.07
                                                                      80
                                                                            1400
                                               697
872
                                        490
                                                      1043
                                                             1320
                                 360
                    70
                          196
   2.85
          2.68
                                                                       8
                                                                            1395
                                                      1216
                                                             1387
                                 452
552
                                        620
          2.54
                   101
                          258
   2.68
                                                                            1361
                                                993
                                                     1274
                                                             1357
                                                                       Δ
                                         745
                          331
          2.43
                   132
   2.54
                                                             1303
                                                                            1304
                                                                       1
                                              1141
                                                      1277
                                 704
                                        910
   2.43
                   192
                          425
          2.34
                                                                       0
                                                                             835
                                                      825
                                                             835
                                        685
                                               787
                   156
                          386
                                 569
   2.34
          2.26
                                                             9545
                                                                    3910
                                                                           13455
                                                      7491
                                       4146
                                              5566
                                3130
                   756
                         1860
 All hkl
                          I/Sigma in resolution shells:
      Shell
                      % of reflections with I / Sigma less than
  Lower Upper
                                                                    >20
                                                              20
                                                                           total
                                                      10
                                 2.7
                                           3
                     0
  limit limit
                                                       9.3
                                                             22.8
                                                                    73.6
                                                                            96.4
                                                5.9
                                         3.9
                          1.9
                   0.8
  99.00
           4.87
                                                                            99.3
                                               6.5
9.2
                                                                    75.2
                                        4.2
                                                      10.8
                                                             24.1
                                 3.3
                          1.9
                   0.8
   4.87
           3.86
                                                                             99.4
                                                             41.3
                                                                    58.1
                                                      19.4
                          2.0
           3.37
                   0.7
    3.86
                                                                            99.5
                                              21.5
                                                      35.2
                                                             61.3
                                                                    38.2
                          5.5
7.3
                                       15.0
                                10.8
    3.37
                   2.4
           3.07
                                                                             99.6
                                                                    14.8
                                                             84.8
                                       20.4
                                               32.6
                                                      56.0
                                14.1
    3.07
           2.85
                   2.6
                                                                            99.7
                                                                     5.7
                                                      74.3
                                                             94.0
                                25.6
                                       34.9
                                               49.6
                         14.0
                   5.0
           2.68
    2.85
                                                             99.0
                                                                     0.6
                                                                             99.6
                                                      86.8
                                       44.3
                                               62.2
                   7.2
                                32.3
           2.54
                         18.4
    2.68
                                                                             99.0
                                                             98.7
                                       54.2
65.7
                                                      92.7
                                                                     0.3
                                40.1
                                               72.2
                         24.1
           2.43
                   9.6
    2.54
                                                                             94.2
                                                             94.1
                                                                     0.1
                                                      92.2
                                               82.4
                         30.7
                                50.8
                  13.9
    2.43
           2.34
                                                                     0.0
                                                                             60.8
                                               57.3
                                                      60.0
                                                             60.8
                                        49.9
                                 41.4
    2.34
                  11.4
                         28.1
           2.26
                                                                             94.8
                                                                    27.6
                                                      52.8
                                                             67.3
                                               39.2
                                        29.2
                         13.1
                                 22.1
                   5.3
 All hkl
                  Summary of reflections intensities and R-factors by shells
      R linear = SUM ( ABS(I - <I>)) / SUM (I)
R square = SUM ( (I - <I>) ** 2) / SUM (I ** 2)
Chi**2 = SUM ( (I - <I>) ** 2) / (Error ** 2 * N / (N-1) ))
      In all sums single measurements are excluded
                                            age Norm. Linear Square
stat. Chi**2 R-fac R-fac
  Shell Lower Upper Average
                                      Average
                             I
                                   error
          Angstrom
  limit
                                                     0.725
                                                                      0.035
                 4.87 \ 10423.\overline{6}
                                             272.0
                                                             0.032
       99.00
                                   333.3
                                                                      0.046
                                                     0.866
                                                             0.041
                                   314.9
                                             262.8
                       10209.3
         4.87
                 3.86
                                                                      0.059
                                                             0.056
                                             190.7
                                                     0.951
                                   234.5
                        5934.8
                 3.37
         3.86
                                                     1.006
                                                                      0.079
                                                             0.081
                        3068.8
1551.7
                                   168.0
                                             150.3
         3.37
                 3.07
                                                             0.131
                                                                      0.126
                                             131.5
                                                     0.972
                                   140.9
                 2.85
         3.07
                                                     1.010
                                                             0.211
                                                                      0.186
                                   129.2
                                             124.8
                          918.7
         2.85
                 2.68
                                                                      0.282
                                                     1.021
                                                             0.311
                                             118.0
                                   122.7
                          581.5
                 2.54
         2.68
                                                             0.388
                                                                      0.348
                                   126.9
                                                     1.086
                                             123.5
                          442.9
                  2.43
         2.54
                                                                      0.466
                                                             0.507
                                                     1.151
                                   142.9
                                             140.9
                          292.8
                  2.34
         2.43
                                                             0.523
                                                     1.056
                                                                      0.457
                                   172.2.
                                             170.3
                          234.8
                  2.26
         2.34
                                                                      0.050
                                             169.9
                                                     0.967
                                                             0.066
                                   191.4
                         3613.0
```

All reflections

#### Table 2

```
Shell
                   I/Sigma in resolution shells:
                     No. of reflections with I / Sigma less than
  Lower Upper
                                                      10
                                                             20
                                                                   >20
                                                                         total
                    0
                                  2
  limit limit
                                                            288
                                        55
                                               84
                                                                  1046
                                                                          1334
                                                     149
          5.16
                   17
                          27
                                 41
  99.00
                                                     127
                                                            235
                                                                          1260
                                        47
                                               71
                                                                  1025
                   11
                          26
                                 38
   5.16
          4.09
                                                            321
                                                                   912
                                                                          1233
                                        65
                                               98
                                                     169
                          29
                                 48
                   15
   4.09
          3.58
                                                            496
                                                                   730
                                                                          1226
                                              160
                                                     270
                   15
                          42
                                 77
                                       106
          3.25
   3.58
                                                                   529
                                                            701
                                                                          1230
                   \overline{27}
                                 99
                                              228
                                                     414
                          62
                                       140
   3.25
          3.02
                                                     574
                                                            925
                                                                   313
                                                                          1238
                                       220
                                              328
                                161
                   41
                         101
   3.02
          2.84
                                                           1052
                                                                   155
                                                                          1207
                                              451
                                                     739
                         125
                                224
                                       308
   2.84
          2.70
                   54
                                                           1155
                                                                    69
                                                                          1224
                                              568
                                                     863
                         187
                                311
                                       399
   2.70
          2.58
                   66
                                                                    54
                                                                          1196
                                                     947
                                                           1142
                                       443
                                              644
                                321
   2.58
          2.48
                   73
                         190
                                                                    22
                                                                          1164
                         250
                                399
                                       552
                                              734
                                                    1006
                                                           1142
                  105
   2.48
          2.39
                                                           7457
                                                                  4855
                                                                         12312
                                                    5258
                                      2335
                                             3366
 All hkl
                  424
                        1039
                               1719
                         I/Sigma in resolution shells:
     Shell
                     % of reflections with I / Sigma less than
  Lower Upper
                                                                  >20
                                                5
                                                           20
                                                                         total
                                  2
                                         3
                                                      10
                    0
                            1
  limit limit
                                                           20.8
                                                                          96.3
                                                                  75.5
                                              6.1
                                                    10.8
                         1.9
                                3.0
                                       4.0
  99.00
          5.16
                  1.2
                                                    10.0
                                                           18.5
                                                                  80.5
                                                                          99.0
                                       3.7
                                              5.6
          4.09
                  0.9
                         2.0
                                3.0
   5.16
                                                                          99.1
                                              7.9
                                       5.2
                                                                  73.3
                         2.3
                                3.9
                                                    13.6
                                                           25.8
                  1.2
   4.09
          3.58
                                                                  59.3
                                                    22.0
                                                           40.3
                                                                          99.7
                         3.4
5.0
                                             13.0
                  1.2
2.2
          3.25
                                6.3
                                       8.6
   3.58
                                                                          99.8
                                                                  42.9
                                             18.5
                                                    33.6
                                                           56.9
                                8.0
                                      11.4
   3.25
          3.02
                                                                  25.2
                                             26.5
                                                    46.3
                                                           74.6
                                                                          99.8
                                      17.7
          2.84
                         8.1
                               13.0
   3.02
                  3.3
                                                                  12.8
                                             37.4
                                                                         100.0
                                                    61.2
                                                           87.2
                  4.5
                        10.4
                               18.6
                                      25.5
   2.84
          2.70
                                                                   5.6
                                                    70.5
                                                           94.4
                                                                         100.0
          2.58
                               25.4
                                      32.6
                                             46.4
   2.70
                  5.4
                        15.3
                                      37.0
                                                                   4.5
                                                    79.2
                                                           95.5
                                                                         100.0
                                             53.8
                        15.9
                               26.8
   2.58
          2.48
                  6.1
                                                                   1.8
                                                                          96.1
                                                    83.1
                                                           94.3
                  8.7
                        20.6
                               32.9
                                      45.6
                                             60.6
   2.48
          2.39
                                                                  39.0
                                                                          99.0
                                                    42.3
                                                           59.9
                                      18.8
                                             27.1
                         8.4
                               13.8
 All hkl
                 Summary of reflections intensities and R-factors by shells
     R linear = SUM ( ABS(I - <I>)) / SUM (I)
R square = SUM ( (I - <I>) ** 2) / SUM (I ** 2)
Chi**2 = SUM ( (I - <I>) ** 2) / (Error ** 2 * N / (N-1) ) )
     In all sums single measurements are excluded
                                                         Linear Square
                                                  Norm.
                                    Average
 Shell Lower Upper Average
                                          stat. Chi**2
                                                          R-fac R-fac
                                 error
 limit
         Angstrom
                                                  0.782
                                                           0.031 0.028
                       3195.0
                                  96.5
                                            34.7
       99.00
                5.16
                                            35.3
                                                                   0.043
                       3070.0
                                                  0.874
                                                           0.041
                                   86.4
        5.16
                4.09
                                                   1.075
                                                                   0.054
                                   63.5
                                            31.6
                                                           0.052
                       2129.1
        4.09
                3.58
                                                           0.069
                                                                   0.067
                                            29.0
        3.58
                                   46.2
                                                   1.164
                3.25
                       1318.2
                                                                   0.103
                                  34.0
                                                   1.312
                                            26.7
                                                           0.108
                        701.0
        3.25
                3.02
                                                   1.209
                                                           0.158
                                                                   0.149
                                            25.6
        3.02
                        424.6
                                   29.1
                2.84
                                                                   0.218
                                                   1.208
                                            24.9
                                                           0.235
                                   26.7
                        272.3
        2.84
                2.70
                                                   1.253
                                                           0.317
                                                                   0.311
                        195.6
                                   25.8
                                            24.6
                2.58
        2.70
                                                                   0.360
                                            25.2
                                                   1.181
                                                           0.369
                                   26.0
        2.58
                2.48
                        164.1
                                            26.5
                                                   1.179
                                                           0.449
                                                                   0.404
                                   27.1
        2.48
                2.39
                        132.9
```

46.9

1192.2

All reflections

28.5

1.122

0.070

0.049

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## 6. Personnel Contributing Effort and Receiving Pay from This Contract

- (i) L. J. DeLucas (10%)
- (ii) S. Narayana (10%)
- (iii) Nasser Iranikah (100%)
- (iv) M. Luo (10%)
- (v) R. Chodavarapu (60%)
- (vi) Alexander Talalaev (50%)
- (vii) Dharmalingam Prahadeeswaran (100%)